



Problem 1: Complex numbers

1. Determine real and imaginary parts

a) $\frac{1-j}{1+j} = -j$ b) $\frac{2}{1-3j} = \frac{1}{5}(1+3j)$ c) $(1+j\sqrt{3})^3 = -8$

2. Determine in polar coordinates

a) $|z| = 3$ and $\varphi = \frac{\pi}{2}$

b) $|z| = 2$ and $\varphi = -\frac{\pi}{2}$

c) $|z| = \sqrt{2}$ and $\varphi = \frac{\pi}{4}$

d) $|z| = \sqrt{2}$ and $\varphi = -\frac{3\pi}{4}$

e) $|z| = \sqrt{29}$ and $\varphi = \arctan\left(\frac{5}{2}\right)$

f) $|z| = \sqrt{29}$ and $\varphi = -\arctan\left(\frac{5}{2}\right)$

g) $|z| = \sqrt{29}$ and $\varphi = \pi - \arctan\left(\frac{5}{2}\right)$

h) $|z| = \sqrt{29}$ and $\varphi = \arctan\left(\frac{5}{2}\right) - \pi$

i) $|z| = |b|$ and $\varphi = \frac{\pi}{2} \operatorname{sgn}(b)$

k) $|z| = \sqrt{a^2 + b^2}$ and $\varphi = \begin{cases} \arctan\left(\frac{b}{a}\right) & , \text{ if } a > 0 \\ \arctan\left(\frac{b}{a}\right) + \pi & , \text{ if } a < 0, b \geq 0 \\ \arctan\left(\frac{b}{a}\right) - \pi & , \text{ if } a < 0, b < 0 \end{cases}$

3. Complex conjugated

Let $z_1 = \frac{1}{2}(1 - \sqrt{3}j)$ and $z_2 = 2e^{j\pi/6}$

a) Compute $z_1 \cdot z_2 = \sqrt{3} - j$

b) Compute $z_1 \cdot \bar{z}_2 = -2j$

c) Determine magnitude and phase of $\bar{z}_1 \cdot z_2 = 2j$

d) Determine real and imaginary part of $\overline{(1+z_1) \cdot (1-\bar{z}_2)} = \frac{3}{2} - \sqrt{3} + j\frac{\sqrt{3}}{2} - j3$

4. Calculate n-th root of a complex number



$$\begin{aligned} \text{a) } \sqrt[3]{j} &= \begin{cases} \frac{\sqrt{3}}{2} + j\frac{1}{2} \\ -\frac{\sqrt{3}}{2} + j\frac{1}{2} \\ -j \end{cases} & \text{b) } \sqrt[4]{-1} &= \begin{cases} \pm \frac{\sqrt{2}}{2}(1+j) \\ \pm \frac{\sqrt{2}}{2}(1-j) \end{cases} \\ \text{c) } \sqrt[6]{-8} &= \begin{cases} \pm \frac{\sqrt{2}}{2}(\sqrt{3}+j) \\ \pm \frac{\sqrt{2}}{2}(\sqrt{3}-j) \\ \pm \sqrt{2}j \end{cases} & \text{d) } \sqrt[8]{1} &= \begin{cases} \pm \frac{\sqrt{2}}{2}(1+j) \\ \pm \frac{\sqrt{2}}{2}(1-j) \\ \pm 1 \\ \pm j \end{cases} \\ \text{e) } \sqrt{1-j} &= \pm \frac{\sqrt{2}}{2} \left(\sqrt{\sqrt{2}+1} - j\sqrt{\sqrt{2}-1} \right) \\ \text{f) } \sqrt{3+4j} &= \pm (2+j) \\ \text{g) } \sqrt[3]{-2+2j} &= \sqrt{2} \left(\cos \left(\frac{2\pi k + \frac{3\pi}{4}}{3} \right) + j \sin \left(\frac{2\pi k + \frac{3\pi}{4}}{3} \right) \right), \quad k = 0, 1, 2 \end{aligned}$$

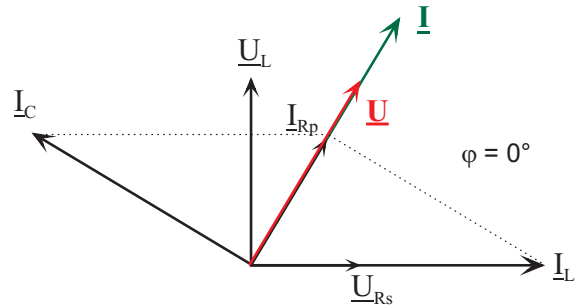
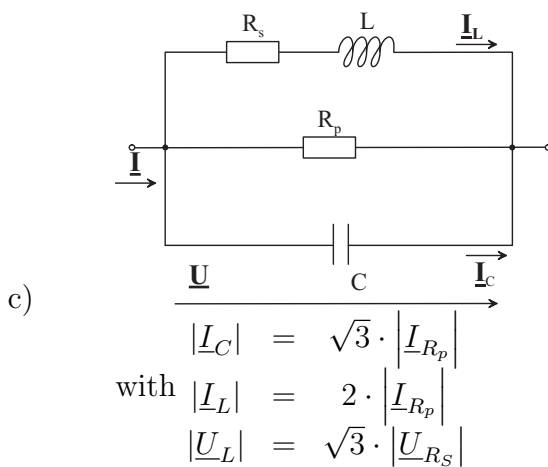
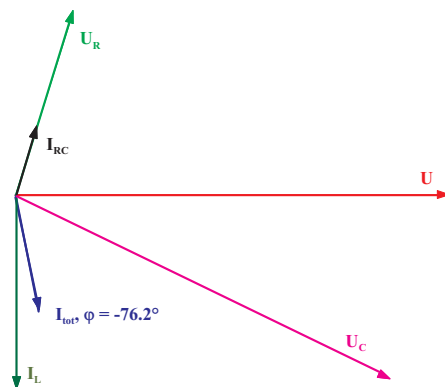
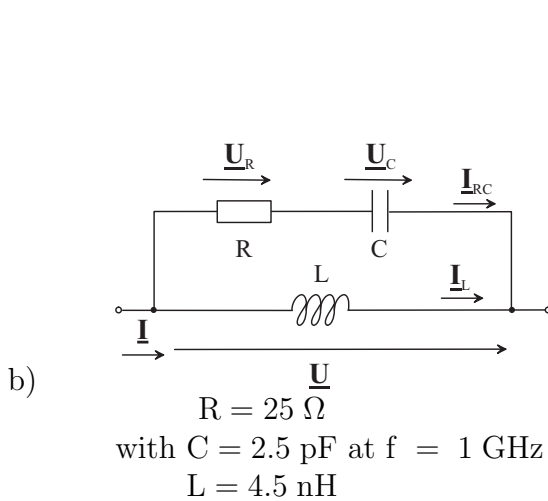
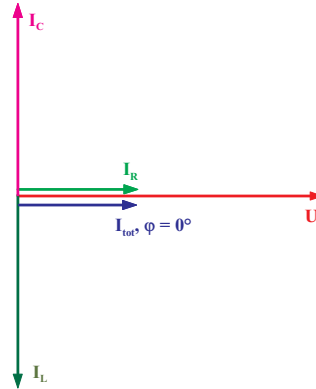
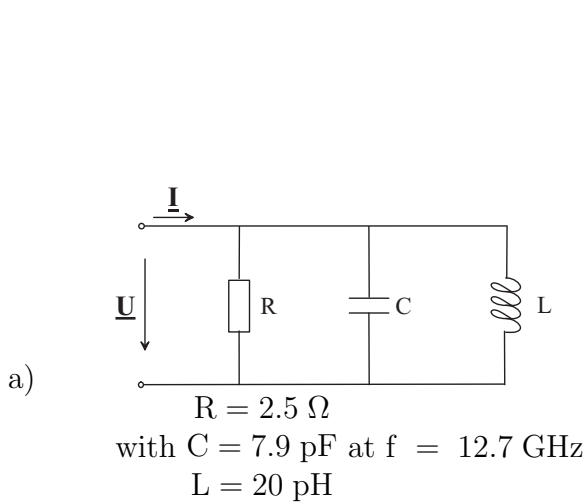
5. Find real and imaginary parts of the following functions

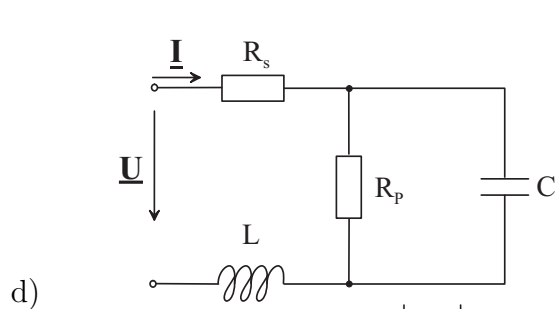
$$\begin{aligned} \text{a) } \cos(2+j) &= \cos 2 \cosh 1 - j \sin 2 \sinh 1 \\ \text{b) } \sin(2j) &= j \sinh 2 \\ \text{c) } \tanh(2-j) &= \frac{\sinh 4 - j \sin 2}{2(\cos^2 2 + \sinh^2 1)} \\ \text{d) } \cot \left(\frac{\pi}{4} - j \cdot \ln 2 \right) &= \frac{8 + j15}{17} \\ \text{e) } \coth(2+j) &= \frac{\sinh 4 - j \sin 2}{\cosh 4 - \cos 2} \end{aligned}$$



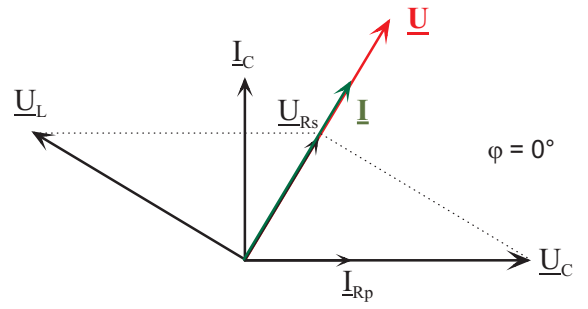
Problem 2: Phasor diagram

Find the phasor diagrams of the given networks and determine the phase shift between the current \underline{I} and the voltage \underline{U} .





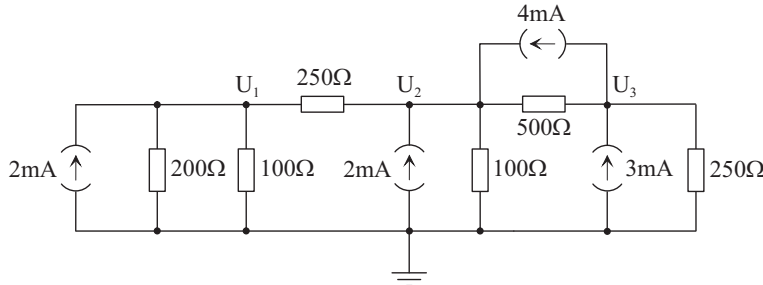
$$\begin{aligned} |I_C| &= \sqrt{3} \cdot |I_{R_p}| \\ \text{with } |U_C| &= 2 \cdot |U_{R_s}| \\ |U_L| &= \sqrt{3} \cdot |U_{R_s}| \end{aligned}$$





Problem 3: Nodal analysis

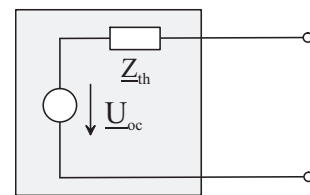
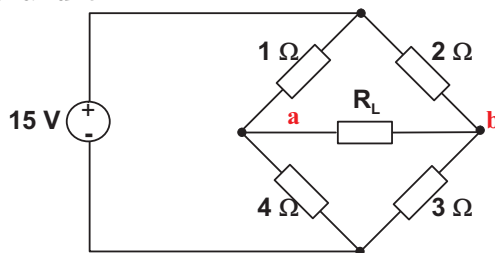
Find the solution of the network given below using nodal analysis. Determine all voltages (U_1 , U_2 , U_3).



$$\begin{bmatrix} U_1 \\ U_2 \\ U_3 \end{bmatrix} = \begin{bmatrix} 0.1937 \\ 0.4201 \\ -0.0266 \end{bmatrix}$$

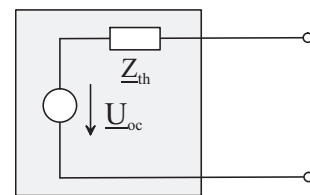
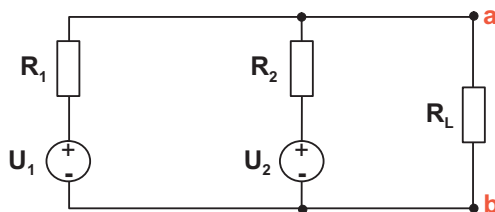
Problem 4: Network theorem

1. Draw a Thévenin equivalent circuit for the circuit in the figure below and determine the value of resistance R_L which will allow a current of 1 A to flow between **a** and **b**.



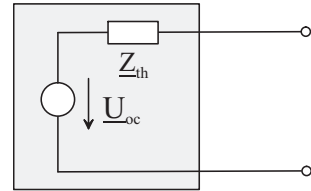
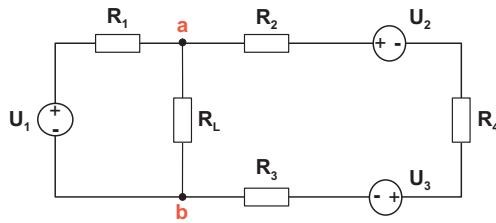
$$U_{oc} = 3 \text{ V}, \underline{Z}_{th} = 2\Omega, R_L = 1\Omega$$

2. Find the Thévenin equivalent circuit for the network to the left of terminals **a** and **b**, if $U_1 = 10 \text{ V}$, $U_2 = 15 \text{ V}$, $R_1 = 4 \Omega$ and $R_2 = 6 \Omega$.

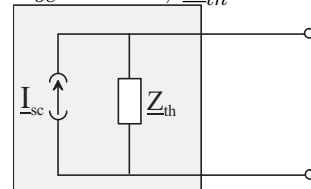


$$U_{oc} = 12 \text{ V}, \underline{Z}_{th} = 2.4\Omega$$

3. Find Thévenin and Norton equivalent circuits for the network between terminals **a** and **b**, if $U_1 = 100 \text{ V}$, $U_2 = 50 \text{ V}$, $U_3 = 10 \text{ V}$, $R_1 = 4 \Omega$, $R_2 = 2.2 \Omega$, $R_3 = 2.3 \Omega$ and $R_4 = 1.5 \Omega$.

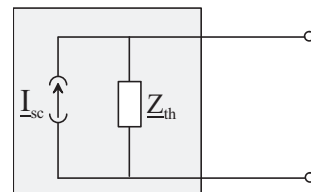
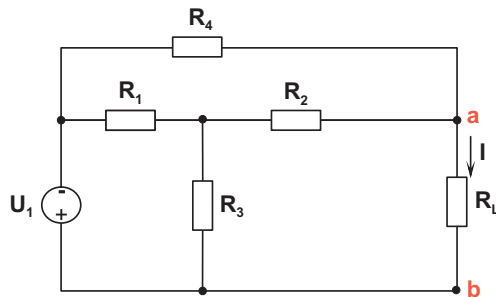


$$U_{oc} = 84 \text{ V}, \underline{Z}_{th} = 2.4\Omega$$



$$I_{sc} = 35 \text{ A}, \underline{Z}_{th} = 2.4\Omega$$

4. Find a Norton equivalent circuit for the network between terminals **a** and **b**, if $U_1 = 2 \text{ V}$, $R_1 = 3 \Omega$, $R_2 = 1 \Omega$, $R_3 = 6 \Omega$ and $R_4 = 6 \Omega$. Use this result to find current I .



$$I_{sc} = -\frac{1}{9} \text{ A}, \underline{Z}_{th} = 2\Omega$$

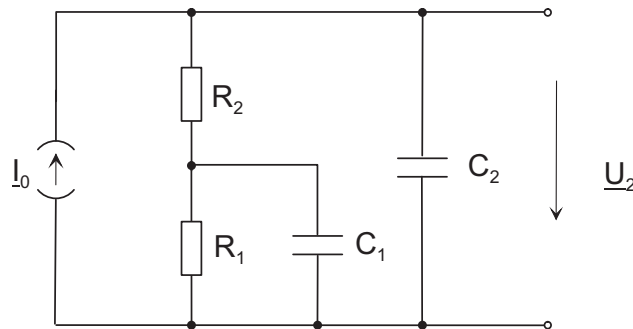
$$I = -\frac{2}{9} \text{ A}$$

Problem 5: Frequency response

In this problem a transfer impedance determined as

$$Z_T(\omega) = \frac{U_2}{I_0}$$

will be studied, where U_2 is the output voltage and I_0 is the source current in the circuit given below.



1. Consider first extreme values of the radian frequency $\omega = 0$ and $\omega = \infty$. Give the expressions for the transfer impedance in these cases. Plot the equivalent circuits at $\omega = 0$ and $\omega = \infty$.

	$\omega = 0$	$\omega \rightarrow \infty$
Equivalent circuit		
$Z_T(\omega) = \frac{U_2}{I_0}$	$R_1 + R_2$	0

2. Give the expression for the complex transfer impedance as a function of the radian frequency ω assuming $R_1 = R_2 = R$ and $C_1 = C_2 = C$.

$$Z_T = \frac{2 \cdot R + j\omega CR^2}{1 - (\omega CR)^2 + j3\omega CR}$$

3. Introduce the normalized frequency $\Omega = \omega \cdot R \cdot C$ and give $Z_T(\Omega)$.



$$\underline{Z}_T = \frac{2 \cdot R + j\Omega R}{1 - \Omega^2 + j3\Omega}$$

4. Give the values of $\underline{Z}_T(\Omega)$ for $\Omega \rightarrow 0$ and $\Omega \rightarrow \infty$.

$$\underline{Z}_T(\Omega = 0) = 2 \cdot R \quad \underline{Z}_T(\Omega \rightarrow \infty) = 0$$

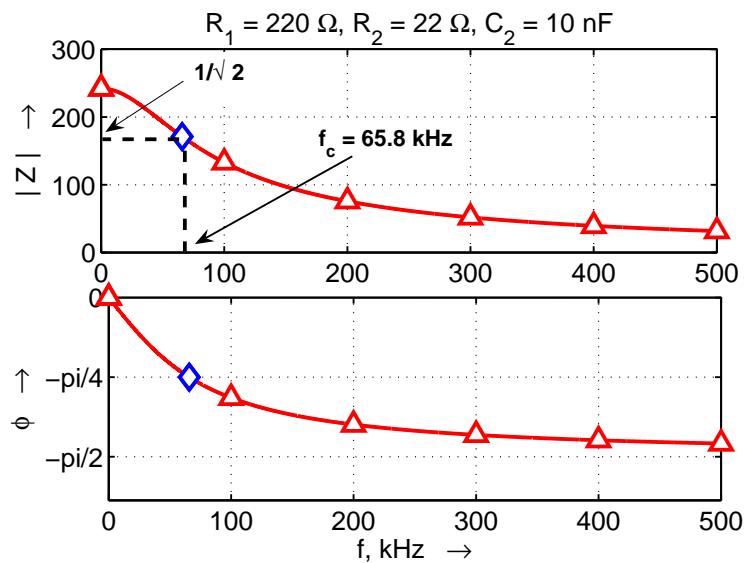
5. Determine the transfer impedance $\underline{Z}_T(\Omega)$ neglecting the capacitance C_1 . Assume that $C_2 = C$ and $R_1 \neq R_2$.

$$\underline{Z}_T = \frac{R_1 + R_2}{1 + j\omega C \cdot (R_1 + R_2)}$$

6. Calculate the 3-dB-corner frequency for circuit configuration of the art before $R_1 = 220 \Omega$, $R_2 = 22 \Omega$ and $C = 10 \text{ nF}$.

$$f_c = \frac{1}{2\pi C \cdot (R_1 + R_2)} = 65.8 \text{ kHz}$$

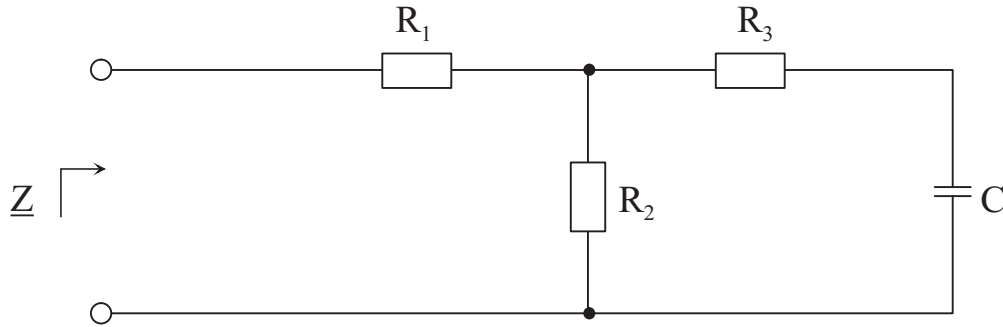
7. Plot the magnitude and the phase of the transfer impedance. Denote on the plot all characteristic points.





Problem 6: Locus diagram

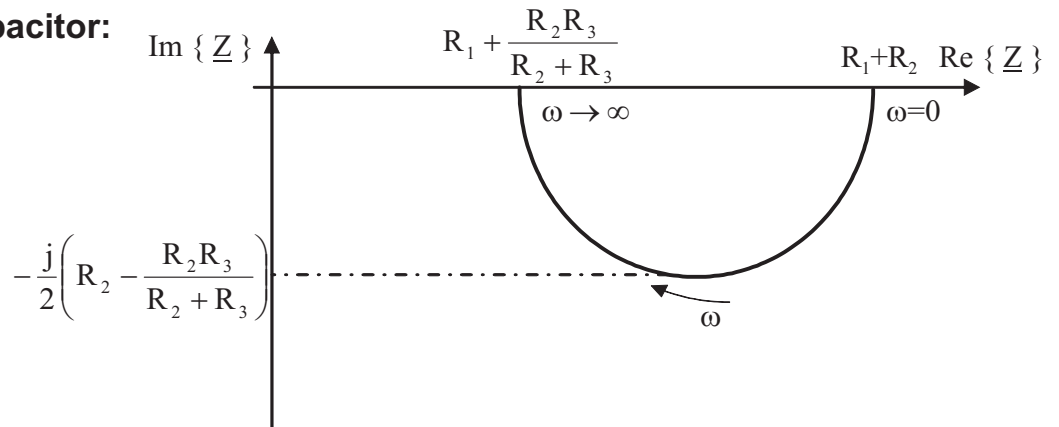
Find the locus diagram for the following circuit:



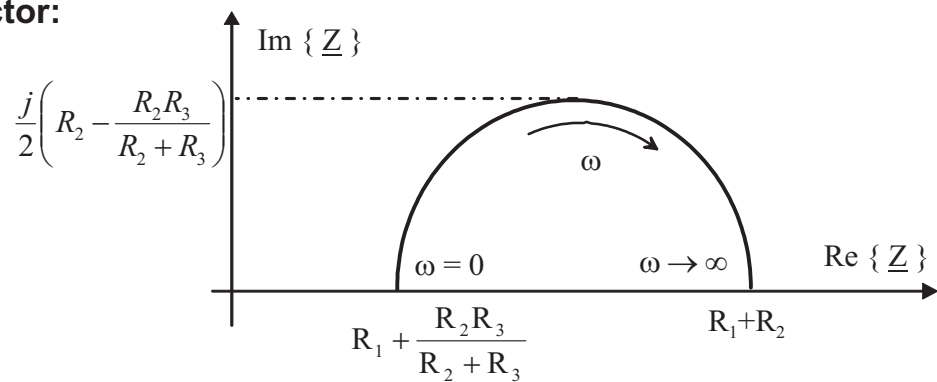
1. Plot stepwise the locus diagram of the circuit with frequency as a parameter.
2. Verify the curve by calculating the impedance directly from the circuit using the frequencies $\omega \rightarrow 0$ and $\omega \rightarrow \infty$.

Answer:

with capacitor:



with inductor:





Problem 7: Resonance

The circuit comprises an ideal sinusoidal current source, a series resistance $R_s = 100 \Omega$ and a parallel resonance circuit with $L = 30 \mu\text{H}$, $C = 0.5 \mu\text{F}$, $R = 10 \Omega$.

1. Find the resonance frequency, bandwidth and quality factor.

$$\omega_0 = 258.2 \cdot 10^3 \frac{\text{rad}}{\text{s}}; B = 220 \cdot 10^3 \frac{\text{rad}}{\text{s}}; Q = 1.17$$

2. Estimate the values of the half-power frequencies.

$$\omega_- = 170.6 \cdot 10^3 \frac{\text{rad}}{\text{s}}; \omega_+ = 390.6 \cdot 10^3 \frac{\text{rad}}{\text{s}}$$

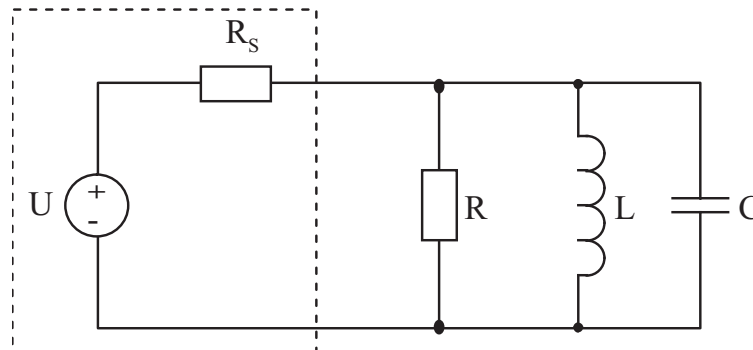
3. What is the influence of a source resistance?

A source resistance decreases the quality of the resonance circuit.

The resonance frequency remains the same $\omega_0 = 258.2 \cdot 10^3$

Without source resistance: $B = 200 \cdot 10^3 \frac{\text{rad}}{\text{s}}; Q = 1.29;$

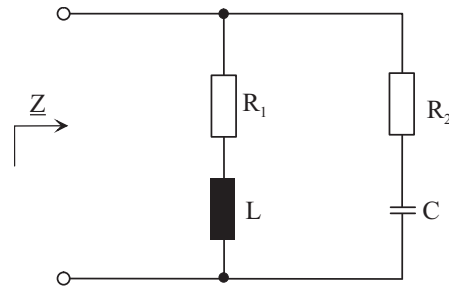
$$\omega_- = 176.0 \cdot 10^3 \frac{\text{rad}}{\text{s}}; \omega_+ = 376.9 \cdot 10^3 \frac{\text{rad}}{\text{s}}$$





Problem 8: Circuit design

Find R_1 , R_2 and C such that the input impedance \underline{Z} for all frequencies equals 100Ω . The inductance L is given $L = 10 \text{ mH}$.



$$R_1 = 100 \Omega$$

$$R_2 = 100 \Omega$$

$$C = 1 \mu\text{F}$$

Corner case 1:

$\omega = 0 \Rightarrow X_L$ - short circuit X_C - open circuit $\Rightarrow \underline{Z} = R_1 = 100 \Omega$

Corner case 2:

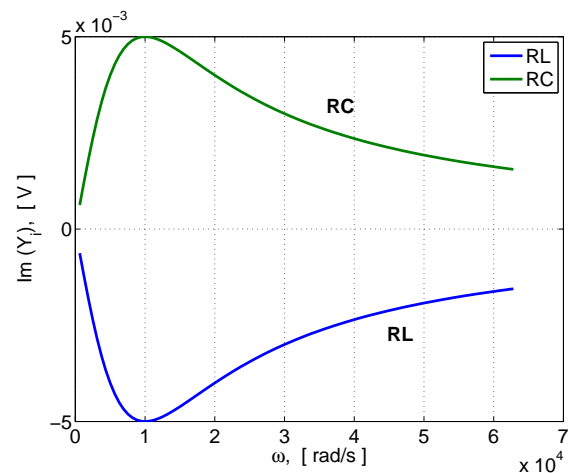
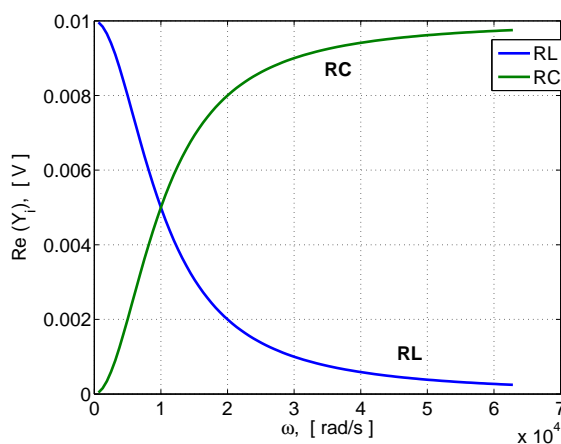
$\omega \rightarrow \infty \Rightarrow X_L$ - open circuit X_C - short circuit $\Rightarrow \underline{Z} = R_2 = 100 \Omega$

Some freq $\omega = \omega_0$:

$$\Rightarrow X_L = -X_C \Rightarrow j\omega_0 L = -\frac{1}{j\omega_0 C}$$

$$100 \Omega = \omega_0 L = \frac{1}{\omega_0 C} \Rightarrow \omega_0 = \frac{X_L}{L}$$

$$C = \frac{1}{\omega_0 X_C} = \frac{L}{X_L^2} \Rightarrow C = 1 \mu\text{F}$$





Problem 9: Two-port (1)

For the circuit shown in the figure below with $R_p = 3 \text{ k}\Omega$, $g_m = 51 \text{ mS}$, $C_1 = 50 \text{ fF}$, $C_2 = 3.2 \text{ fF}$ and $C_3 = 34 \text{ fF}$ at $f = 0.5 \text{ GHz}$

1. calculate the Y-parameters;

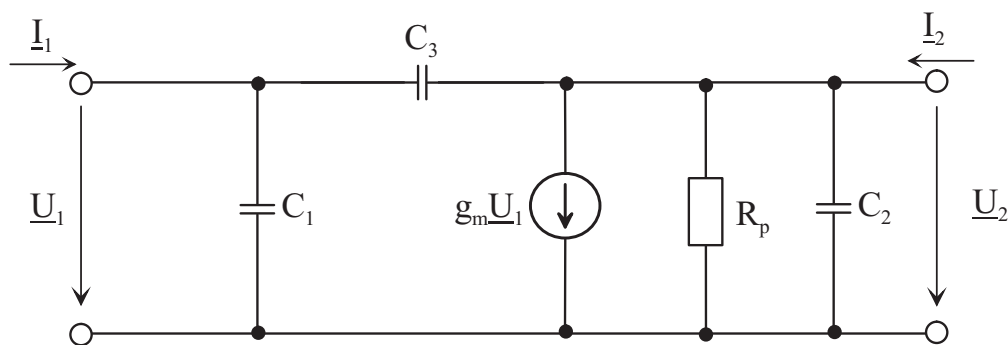
$$[\underline{Y}] = \begin{bmatrix} j\omega \cdot (C_1 + C_3) & -j\omega C_3 \\ g_m - j\omega C_3 & \frac{1}{R_p} + j\omega (C_2 + C_3) \end{bmatrix}$$

2. compare the voltage gain $\underline{U}_2/\underline{U}_1$ for $R_L = 50 \Omega$ and $R_L = \infty$.

$$\underline{G}_V = \frac{\underline{U}_2}{\underline{U}_1} = - \frac{g_m - j\omega C_3}{\frac{1}{R_p} + j\omega (C_2 + C_3) + \frac{1}{R_L}}$$

$$\left| \underline{G}_V (R_L = 50\Omega) \right| = 2.5 \hat{=} 8 \text{ dB}$$

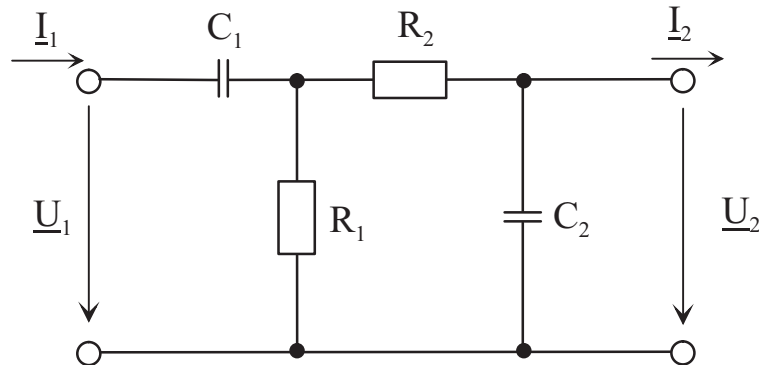
$$\left| \underline{G}_V (R_L \rightarrow \infty) \right| = 153 \hat{=} 44 \text{ dB}$$





Problem 10: Two-port (2)

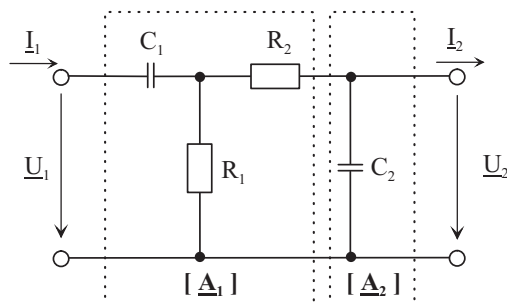
Determine the chain parameters of the two-port shown in the figure below:



1. using chain parameter definition;

$$[\underline{A}] = \begin{bmatrix} 1 + j\omega C_2 \cdot R_2 + \frac{1 + j\omega C_2 (R_1 + R_2)}{j\omega C_1 R_1} & R_2 + \frac{1}{j\omega C_1} \cdot \left(1 + \frac{R_2}{R_1}\right) \\ \frac{1}{R_1} + j\omega C_2 \cdot \left(1 + \frac{R_2}{R_1}\right) & 1 + \frac{R_2}{R_1} \end{bmatrix}$$

2. using two sub-circuits in cascade connection.



$$[\underline{A}_1] = \begin{bmatrix} 1 + \frac{1}{j\omega C_1 R_1} & R_2 + \frac{1}{j\omega C_1} + \frac{R_2}{j\omega C_1 R_1} \\ \frac{1}{R_1} & 1 + \frac{R_2}{R_1} \end{bmatrix}$$

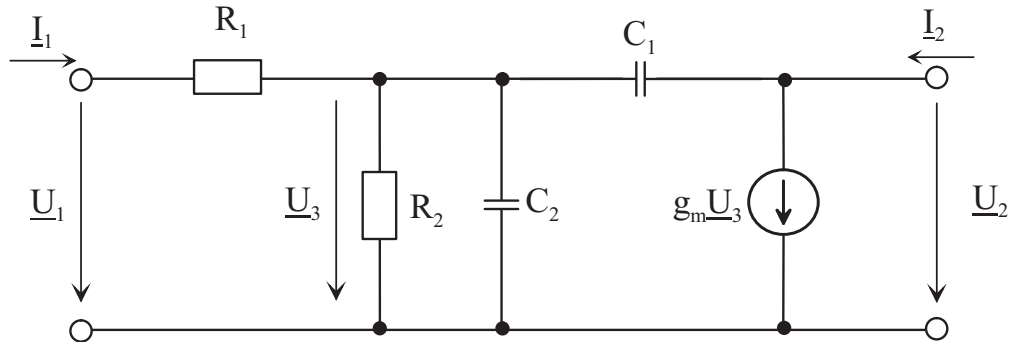
$$[\underline{A}_2] = \begin{bmatrix} 1 & 0 \\ j\omega C_2 & 1 \end{bmatrix}$$

$$[\underline{A}] = [\underline{A}_1] \cdot [\underline{A}_2]$$



Problem 11: Two-port (3)

A small-signal equivalent circuit of a bipolar transistor in common-emitter configuration is shown in figure below. Determine the h-parameters of the given two-port.



$$[H] = \begin{bmatrix} R_1 + \frac{1}{\frac{1}{R_2} + j\omega(C_1 + C_2)} & \frac{j\omega C_1}{\frac{1}{R_2} + j\omega C_1 + j\omega C_2} \\ \frac{g_m - j\omega C_1}{\frac{1}{R_2} + j\omega(C_1 + C_2)} & j\omega C_1 \cdot \frac{g_m - j\omega C_1}{\frac{1}{R_2} + j\omega(C_1 + C_2)} + j\omega C_1 \end{bmatrix}$$



Problem 12: Transistor models

1. An NMOS transistor has the following parameters:

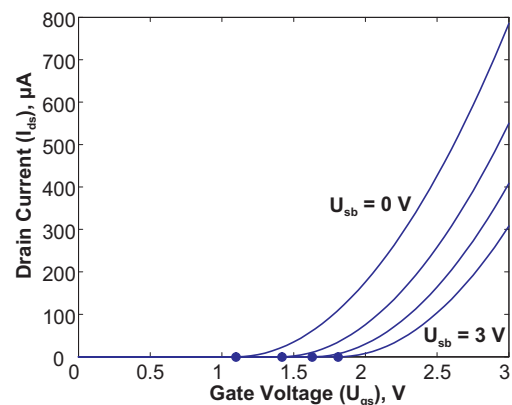
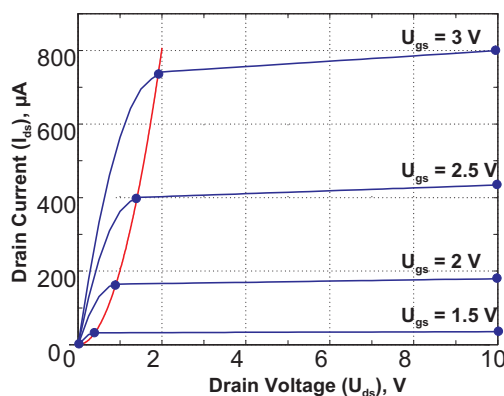
$$\begin{array}{ll}
 W = 100 \mu\text{m} & L = 10 \mu\text{m} \\
 \lambda = 0.01\text{V}^{-1} & \mu_n = 1400 \text{ cm}^2/(\text{V} \cdot \text{s}) \\
 t_{\text{ox}} = 0.12 \mu\text{m} & \phi_f = 0.3 \text{ V} \\
 N_A = 10^{15} \text{ atom/cm}^3 & \epsilon_{\text{Si}} = 11.7 \\
 \epsilon_{\text{ox}} = 3.9 & \epsilon_0 = 8.854 \cdot 10^{-15} \text{ F/m} \\
 U_{\text{to}} = 1.1 \text{ V} &
 \end{array}$$

a) Sketch the $I_{\text{ds}}-U_{\text{ds}}$ characteristics for U_{ds} from 0 to 10 V and $U_{\text{gs}} = 1.5, 2, 2.5$ and 3 V. Assume $U_{\text{sb}} = 0$ V.

U_{gs}, V	1.5	2	2.5	3
U_{ds}, V	0.4	0.9	1.4	1.9
$I_{\text{ds}}, \mu\text{A}$	32.23	163.16	394.81	727.17
U_{gs}, V	1.5	2	2.5	3
U_{ds}, V	10	10	10	10
$I_{\text{ds}}, \mu\text{A}$	35.45	179.48	434.29	799.89

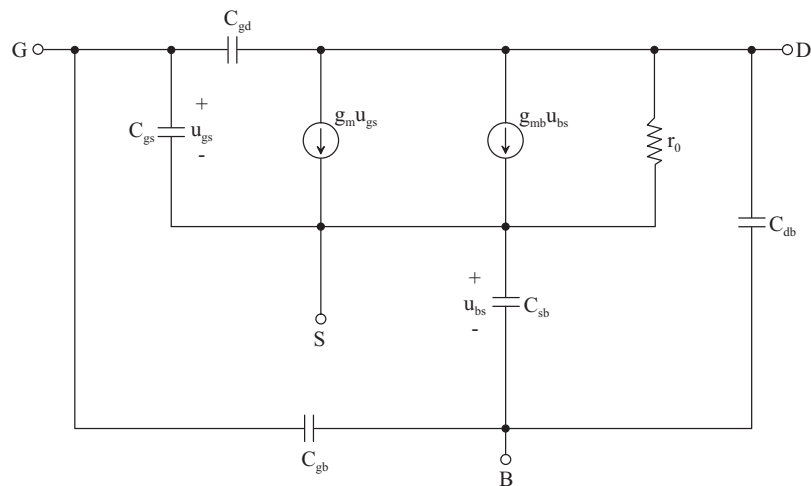
b) Sketch the $I_{\text{ds}}-U_{\text{gs}}$ characteristics for $U_{\text{ds}} = 8$ V as U_{gs} varies from 0 to 3 V with $U_{\text{sb}} = 0, 1, 2$ and 3 V.

U_{sb}, V	0	1	2	3
U_{th}, V	1.1	1.41	1.63	1.81





2. Derive and sketch the complete small-signal equivalent circuit for the device of Problem 1 with $U_{gs} = 2 \text{ V}$, $U_{ds} = 10 \text{ V}$, and $U_{sb} = 1 \text{ V}$. Use $\psi_0 = 0.6 \text{ V}$, $C_{sb0} = C_{db0} = 0.2 \text{ pF}$, $C_{gb} = 0.08 \text{ pF}$. Overlap capacitance from gate to source and gate to drain is 0.02 pF .



$$\begin{array}{ll} g_m = 0.26 \text{ mS} & C_{db} = 45.4 \text{ fF} \\ g_{mb} = 66 \text{ } \mu\text{S} & C_{gs} = 211 \text{ fF} \\ r_0 = 1.3 \text{ M}\Omega & C_{gd} = 20 \text{ fF} \\ C_{sb} = 122 \text{ fF} & C_{gb} = 80 \text{ fF} \end{array}$$

3. Use the device data of Problems 1 and 2 to calculate the frequency of unity current gain of the transistor with $U_{ds} = 5 \text{ V}$, $U_{sb} = 0 \text{ V}$, and $U_{gs} = 1.5, 2$ and 3 V .

$U_{gs}, \text{ V}$	1.5	2	3
$f_t, \text{ MHz}$	86	194	410

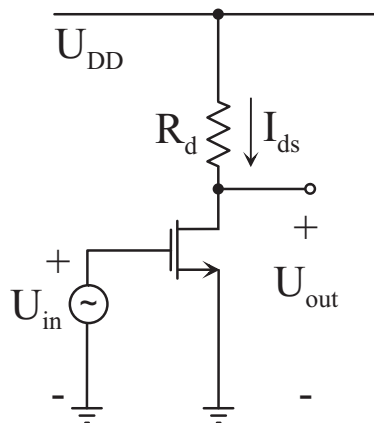


Problem 13: Basic Single Transistor Amplifier Stage

For the common-source amplifier of the figure below calculate the small-signal voltage gain and the bias values of U_{in} and U_{out} at the edge of the triode region. Also calculate the bias values of U_{in} and U_{out} where the small-signal voltage gain is unity.

Assume:

$$\begin{aligned} U_{DD} &= 5 \text{ V} & \lambda &= 0 \text{ V}^{-1} \\ \mu_n \cdot C'_{ox} &= 40 \text{ } \mu\text{A}/\text{V}^2 & U_{th} &= 0.8 \text{ V} \\ W &= 100 \text{ } \mu\text{m} & R_D &= 5 \text{ k}\Omega \\ L &= 10 \text{ } \mu\text{m} \end{aligned}$$



1. Calculate the small-signal voltage gain and the bias values of U_{in} and U_{out} at the edge of the triode region.

$$\begin{aligned} U_{ds} &= 1.79 \text{ V} \\ U_{gs} &= 2.6 \text{ V} \\ G_V &= -3.58 \text{ V} \end{aligned}$$

2. Calculate the bias values of U_{in} and U_{out} where the small-signal voltage gain is unity.

$$\begin{aligned} U_{ds} &= 4.75 \text{ V} \\ U_{gs} &= 1.3 \text{ V} \end{aligned}$$

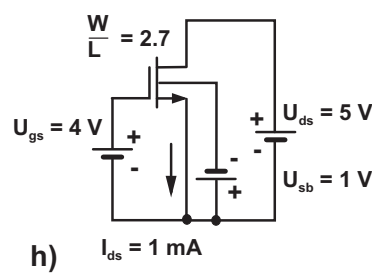
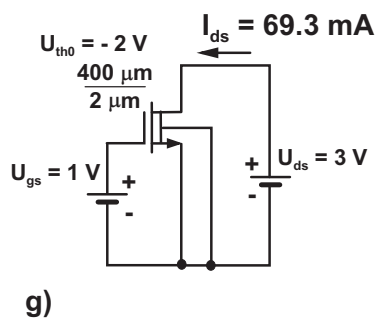
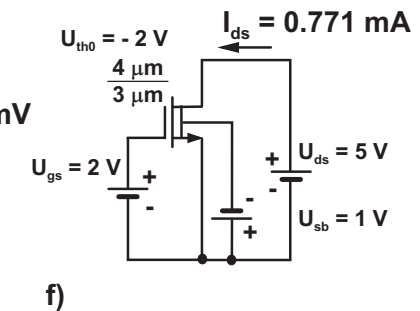
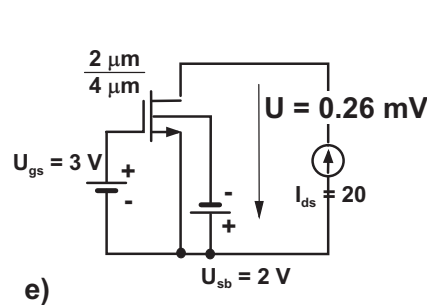
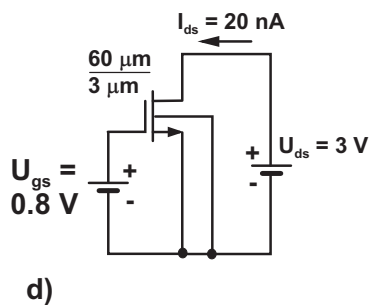
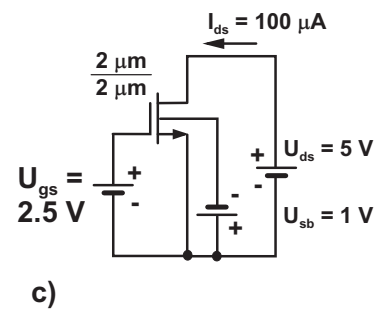
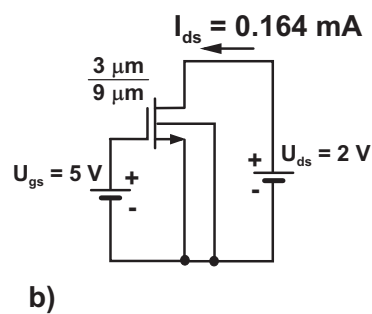
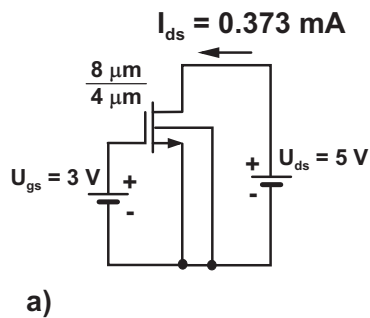


Problem 14: nMOS Transistors

Calculate the quantities indicated in the figure below, assuming the following parameters:

$$\mu_n \cdot C_{ox} = 77 \mu\text{A}/\text{V}^2, U_{th,0} = 0.8 \text{ V}, \phi_f = 0.76 \text{ V}, \gamma = 0.35 \text{ V}^{1/2} \text{ and } \lambda = 0 \text{ V}^{-1}$$

The quantities next to the devices in a form a/b mean $W = a$ and $L_g = b$.

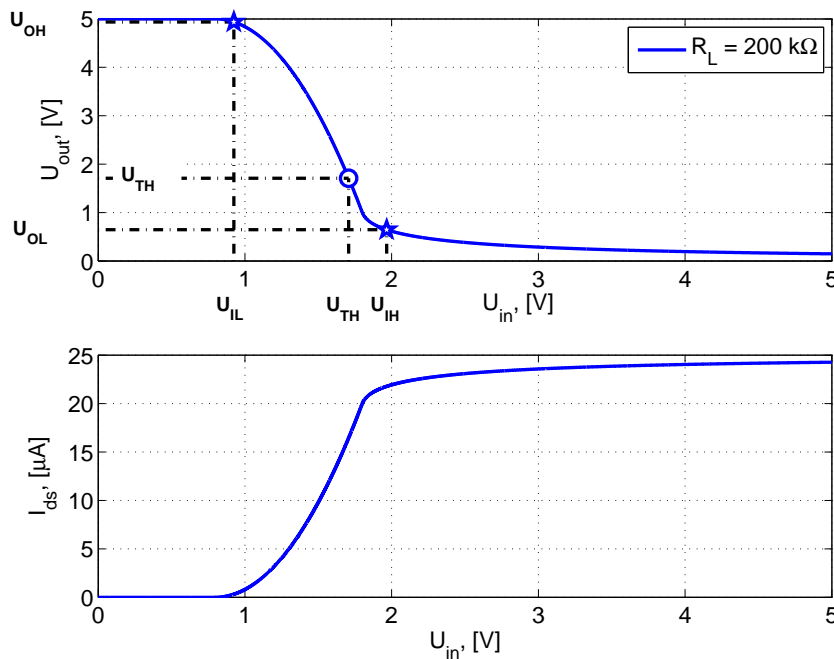




Problem 15: Resistive-load inverter

Consider a resistive-load inverter circuit with $k_n = 40 \mu\text{A}/\text{V}^2$, $U_{th,0} = 0.8 \text{ V}$, $R_L = 200 \text{ k}\Omega$ and $U_{DD} = 5 \text{ V}$.

1. Sketch the voltage transfer characteristics of the inverter and calculate the critical points (U_{OL} , U_{OH} , U_{IL} and U_{IH}).



$$\begin{aligned} U_{OL} &= 0.147 \text{ V} \\ U_{IL} &= 0.925 \text{ V} \\ U_{IH} &= 1.97 \text{ V} \\ U_{OH} &= 5 \text{ V} \\ U_{TH} &= 1.7 \text{ V} \end{aligned}$$

2. Find the noise margins of the circuit. Comment the quality of the inverter.

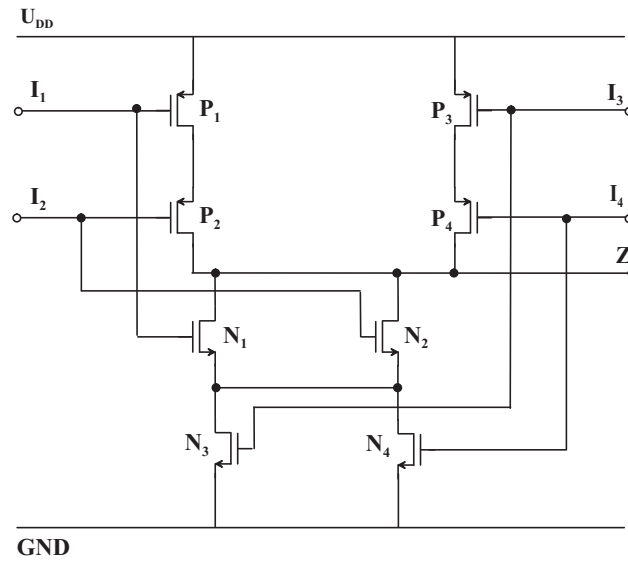
$$\begin{aligned} NM_L &= 0.28 \text{ V} \\ NM_H &= 2.97 \text{ V} \\ NM_L &\text{ is too low.} \\ &\text{It should be about 25\% of } U_{DD}. \end{aligned}$$



Problem 16: Digital CMOS Circuits

Create truth tables and transistor-level schematics using CMOS logic gates for the following functions:

1. $\bar{Q} = [I_1 + I_2] \cdot [I_3 + I_4]$



2. $Z = (\bar{I}_1 \cdot \bar{I}_2) + \bar{I}_3 + \bar{I}_4$

